

Designing reforming catalysts for biomass derived syngas conditioning for fuel synthesis

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Introduction

The efficient thermochemical gasification of biomass to syngas for liquid fuels production requires the use of a catalytic steam reforming process to remove tars. This approach to produce clean syngas additionally maximizes the use of the biomass carbon and hydrogen content. The catalysts used in the steam reforming reactor can comprise a significant portion of the overall process cost to produce biofuels. In order to reduce the catalyst cost and improve the overall fuel synthesis economics, highly active and stable catalysts are required. To achieve this goal, we are using rational catalyst design to understand, design, and synthesize robust, multi-functional catalysts capable of handling biomass-derived impurities such as tars, polyaromatic hydrocarbons (PAHs), and H₂S. Results of catalyst performance are discussed.

Materials and Methods

The catalysts were prepared via incipient wetness impregnation. The support material consisted of a hard, attrition-resistant spray dried alumina designed for operating in a fluidized bed reactor (CoorsTek). The catalyst preparation parameters that were varied included Ni, Mg, and K content and the addition of a 2nd metal. These compositions were based on commercial reforming catalyst compositions that demonstrated good reforming performance but attrited significantly under fluidized bed operations. Five sets of NREL catalysts were created with low, medium, and high levels of magnesium oxide and potassium oxide. Each set had a different nickel loading. A sixth set consisted of four catalysts containing a second metallic species. Precursor materials used in the preparation of these catalysts comprised nitrate salts: Ni (NO₃)₂·6H₂O, Mg (NO₃)₂·6H₂O, and KNO₃ (Alfa Aesar). One step impregnation of the supports was conducted with addition of an aqueous solution of the salts to incipient wetness followed by calcination in air at 650 °C for two hours to convert the salts to oxides. Prior to use, all catalysts were reduced in flowing hydrogen at reaction temperature (850 °C).

Reaction experiments to assess catalyst steam reforming activity were conducted with 1) ethylene as a surrogate tar, 2) ethylene in model syngas containing hydrogen sulfide, and 3) ethylene after steam regeneration in a microactivity test system (MATs)¹ equipped with a rapid scanning gas chromatograph (Varian Micro) that measured permanent gases, hydrocarbons, and sulfur species contained in the process gas. Steam regeneration and hydrogen reduction were conducted after each reforming reaction to regenerate the sulfided catalyst surface and reduce NiO to Ni, respectively, prior to evaluating further reforming performance. Regeneration was conducted at 850 °C in steam for 1 hour with subsequent reduction occurring at the same temperature in 10% H₂ in He for 1 hour. Initial performance was obtained in pure ethylene and differential performance in model biomass derived syngas containing CO, CO₂, H₂, CH₄, C₂H₄, and C₆H₆.

Results and Discussion

Results from the initial catalyst screening phase are summarized in Table 1. In general, catalysts doped with magnesium oxide performed better than those without magnesium oxide. Those catalysts with a ratio of NiO:MgO of ~2:1 showed higher conversion of ethylene than catalysts with the same NiO content and other MgO loadings. The previously studied NREL Catalyst 32a, which has been used with raw syngas, was used as a benchmark to compare catalyst activity for the initial screening phase. The addition of other metallic species improved catalyst regenerability after reaction in hydrogen sulfide.

Table 1: Ethylene conversion obtained with varied Ni-alumina steam reforming catalysts.

| Catalyst | % C ₂ H ₄ Conversion ¹ | % C ₂ H ₄ Conversion ² | %C ₂ H ₄ Conversion ³ | % C ₂ H ₄ Conversion ^{4,5} | |
|----------|--|--|---|--|----|
| Cat 34a | 30 | 20 | 18 | | |
| Cat 34b | 19 | 19 | 48 | | |
| Cat 34c | 52 | 70 | 95 | | |
| Cat 34d | 37 | 37 | 37 | | |
| Cat 34e | 96 | 43 | 100 | | |
| Cat 34f | 91 | 37 | 69 | 85 | 78 |
| Cat 34g | 80 | 30 | 87 | | |
| Cat 34h | 82 | 21 | 82 | | |
| Cat 34i | 78 | 16 | 76 | | |
| Cat 34j | 94 | 55 | 30 | | |
| Cat 34k | 86 | 58 | 95 | | |
| Cat 34l | 88 | 38 | 92 | | |
| Cat 34m | 98 | 73 | 100 | 87 | 90 |
| Cat 34n | 95 | 49 | NA | 88 | 82 |
| Cat 34o | 93 | 53 | 100 | 78 | 90 |
| Cat 35a | 79 | 12 | 79 | | |
| Cat 35b | 68 | 20 | 71 | | |
| Cat 35c | 61 | 8 | 60 | | |
| Cat 35d | 82 | 16 | 82 | | |
| Cat 32a | 97 | 13 | 98 | 83 | 79 |

¹ Steady state ethylene steam reforming ² in 20 ppmv H₂S; ³ after steam regeneration and hydrogen reduction; ⁴ in model syngas; and ⁵ in model syngas after regeneration from reforming with 20 ppm H₂S.

Significance

This work demonstrates the optimum composition of a fluidizable Ni-Mg-K-alumina catalyst for reforming tars contained in biomass derived syngas.

References

1. Magrini-Bair, K., Czernik, S., French, R., Parent, Y., Chornet, E., Dayton, D., Feik, C., Bain, R. Applied Catalysis 318, 199-206 (2007).