# Potential of $NO_{\rm X}$ storage/release materials for high temperature diesel soot oxidation

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## Introduction

Particulate matter (soot) and  $NO_X$  are the main pollutants in diesel engine emissions and represent health and environmental problems. In Euro V emission standards for cars and light trucks, which are expected to be implemented in 2009, level of soot in exhaust should be decreased almost five times in comparison with Euro IV regulations¹. Normally soot can be oxidised by oxygen to  $CO+CO_2$  around  $600^{\circ}C$ . During most of the diesel engine operations the exhaust gas temperature is below  $300^{\circ}C$  which is too low to initiate continuous uncatalysed soot oxidation. Soot is, therefore, collected on a filter and further can be oxidised at high temperatures to regenerate the filter. To improve fuel economy the duration of the regeneration interval should be as short as possible and it should at the same time ensure complete trap regeneration.

Since  $NO_2$  is a more powerful oxidant than oxygen, a possible strategy is to use a combination of a  $NO_X$  storage material which will store the  $NO_X$  at temperatures below 300°C as nitrates and release it at the temperature of regeneration<sup>2,3</sup>. An oxidation catalyst will oxidize NO into  $NO_2$  and subsequently the  $NO_2$  will convert soot selectively into  $CO_2$  and back to NO

as schematically shown in the Figure 1. As NO<sub>x</sub> storage materials, alkali, alkali-earth and rare-earth oxides have clearly potential, since they can store NO<sub>x</sub> in form of nitrates and nitrites low at temperatures and release it as NO. NO2. and active oxygen upon heating.

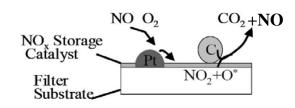


Figure 1: Soot oxidation on the filter combining  $NO_{\rm X}$  storage material and oxidation catalyst.

# **Experimental**

A large variety of mono and bimetallic  $NO_X$  storage/release systems supported on  $Al_2O_3$ ,  $ZrO_2$  and  $CeO_2$  have been prepared. In most cases Pt was added to oxidize NO into  $NO_2$ . Textural properties of resulting catalysts were studied using  $N_2$  adsorption measurements, XRD, and TGA.  $NO_X$  storage/release behavior was analyzed as a function of temperature by FTIR and by temperature programmed desorption (TPD) both coupled with a MS. Soot oxidation was studied both in isothermal and temperature-programmed conditions.

# **Results and Discussion**

For alkali-earth and rare-earth based systems NO<sub>X</sub> storage capacity was found to be significantly lower than theoretical calculated assuming 100% nitrate formation for storage component. For alkali-earth based systems the NO<sub>X</sub> storage capacity increases on going from Ba via Sr and Ca to Mg while the stability of formed nitrates decreases. The pretreatment conditions and temperature of NO<sub>X</sub> storage also have a significant effect on the storage capacity. The presence of soot decreases the temperature of NO<sub>x</sub> release. The main product of nitrates decomposition in the presence of soot is nitrogen monoxide and NO has a significantly smaller effect on soot oxidation than NO<sub>2</sub>. Therefore, the presence of oxidation catalyst is beneficial. It is found that even above 450°C, where NO conversion to NO2 is thermodynamically unfavorable, the presence of small amounts of NO<sub>2</sub> has a very strong positive effect on soot oxidation due to high recycle efficiency of NO into NO2. In this case soot is oxidized through two parallel paths; oxidation with NO<sub>2</sub> and oxidation with oxygen. Heat produced during soot oxidation by NO<sub>2</sub> can be utilized to initiate soot oxidation with oxygen. The presence of stored NO<sub>x</sub> does not influence soot oxidation selectivity, while the presence of oxidation catalyst increases selectivity to CO2 significantly. These trends are illustrated here on the example of Sr-based system and the main results are summarized in Table 1.

**Table 1.** Soot oxidation with air in the presence of NO<sub>X</sub> storage/release system.

System	T <sub>max1</sub> , °C*	$T_{max2}$ , °C**	S <sub>1</sub> , %***	T <sub>20%</sub> , °C	S <sub>CO2</sub> , %
20%Sr(NO <sub>3</sub> ) <sub>2</sub> /Al <sub>2</sub> O <sub>3</sub>	552	-	-	-	-
soot+Al <sub>2</sub> O <sub>3</sub> (1:20)	-	633	0	584	88
soot+1%Pt/Al <sub>2</sub> O <sub>3</sub> (1:20)	-	613	0	565	93
soot+20%Sr(NO <sub>3</sub> ) <sub>2</sub> /Al <sub>2</sub> O <sub>3</sub>	507	643	5.2	539	85
soot+20%Sr(NO <sub>3</sub> ) <sub>2</sub> /Al <sub>2</sub> O <sub>3</sub>	503	610	9.1	509	86
soot+1%Pt-20%Sr(NO <sub>3</sub> ) <sub>2</sub> /Al <sub>2</sub> O <sub>3</sub>	467	591	34.9	484	97

<sup>\*</sup> temperature of the maximum for NO<sub>x</sub> assisted soot oxidation (correlate with temperature of NO<sub>x</sub> release)

## Conclusions

It is shown that the combination of  $NO_X$  storage/release component and oxidation catalyst enables to decrease time and the temperature of the diesel soot oxidation significantly which would result in lower fuel penalty for the soot filter regeneration.

#### References

- http://www.dieselnet.com/standards/
- 2. A. Setiabudi, M. Makkee, J.A. Moulijn, Appl. Catal. B, 50 (2004) 185.
- 3. K. Krishna, M. Makkee, Catal. Today, 114 (2006) 48.

<sup>\*\*</sup> temperature of the maximum for soot oxidation with oxygen

<sup>\*\*\*</sup> share of NOx assisted soot oxidation in overall soot conversion